The QSSA in Chemical Kinetics: As Taught and as Practiced

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Abstract Chemical mechanisms for even simple reaction networks involve many highly reactive and short-lived species (intermediates), present in small concentrations, in addition to the main reactants and products, present in larger concentrations. The chemical mechanism also often contains many rate constants whose values are unknown a priori and must be determined from experimental measurements of the large species concentrations. A classic model reduction method known as the quasi-steady-state assumption (QSSA) is often used to eliminate the highly reactive intermediate species and remove the large rate constants that cannot be determined from concentration measurements of the reactants and products. Mathematical analysis based on the QSSA is ubiquitous in modeling enzymatic reactions. In this chapter, we focus attention on the QSSA, how it is "taught" to students of chemistry, biology, and chemical and biological engineering, and how it is "practiced" when researchers confront realistic and complex examples. We describe the main types of difficulties that appear when trying to apply the standard ideas of the OSSA. and propose a new strategy for overcoming them, based on rescaling the reactive intermediate species.

First, we prove mathematically that the program taught to beginning students for applying the 100-year-old approach of classic QSSA model reduction *cannot*

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be carried out for many of the relevant kinetics problems, and perhaps even most of them. By using Galois theory, we prove that the required algebraic equations cannot be solved for as few as five bimolecular reactions between five species (with three intermediates). We expect that many practitioners have suspected this situation regarding nonsolvability to exist, but we have seen no statement or proof of this fact, especially when the kinetics are restricted to unimolecular and bimolecular reactions. We describe algorithms that can test any mechanism for solvability. We also show that an alternative to solving the QSSA equations, the Horiuti–Temkin theory, also does not work for many examples.

Of course, the reduced model (and the full model, for that matter) can be solved numerically, which is the standard approach in practice. The remaining difficulty, however, is how to obtain the values of the large kinetic parameters appearing in the model. These parameters *cannot* be estimated from measurements of the large-concentration reactants and products. We show here how the concept of rescaling the reactive intermediate species allows the large kinetic parameters to be removed from the parameter estimation problem. In general, the number of parameters that can be removed from the full model is less than or equal to the number of intermediate species. The outcome is a reduced model with a set of rescaled parameters that is often identifiable from routinely available measurements. New and freely available computational software (parest_dae) for estimating the reduced model's kinetic parameters and confidence intervals is briefly described.

1 Introduction

The quasi-steady-state assumption (QSSA) has become a cornerstone of chemical kinetic modeling and model reduction since its introduction almost a 100 years ago [4,5]. Typical kinetic mechanisms describing any reasonably complex chemical system involve species that have large concentrations, namely the reactants and products, and species that have vanishingly small concentrations, usually referred to as reactive intermediates or simply intermediates. The reactive intermediates have small concentrations because their rates of formation are small compared with their rates of consumption over the range of species concentrations of interest. Models that contain highly reactive intermediates usually display a behavior with two (or more) timescales. The full model exhibits a fast timescale, during which the highly reactive intermediates change from their starting conditions (often zero) to quasi-steady values relative to the reactants and products, and a slow timescale, during which the large-concentration reactants and products evolve. The QSSA is used to remove the highly reactive, low-concentration species from the model and produce a reduced model valid on the slow timescale, which is usually the timescale of interest for analyzing measurements, identifying reduced mechanisms, estimating model parameters, and designing experiments and industrial reactors. As taught in introductory examples, the QSSA reduced model usually contains only the reactants and products. The rate expressions for the production and consumption of reactants

and products in terms of only the reactants and products are called the reduced mechanism. Like the QSSA itself, the reduced mechanism is valid over the usual range of species concentrations exhibited by the chemical system of interest.

The quasi-steady-state assumption is widely used in modeling enzymatic reactions, where the intermediates are various enzyme–substrate complexes. The QSSA is at the core of most enzyme kinetics models, such as the Michaelis–Menten kinetics for the basic enzyme reaction [18, 20], the Hill kinetics for cooperative enzymatic models [11, 18], models for enzyme inhibition processes [18], and the Goldbetter–Koshland function in models of futile cycles [9, 24].

The model reduction provides several advantages.

- Model validation. The reduced mechanism allows the model developer to test
 the structure of the mechanism against experimental measurements. Since the
 reduced mechanism involves only the more easily measured high-concentration
 reactants and products, the experimental measurements and therefore the model
 validation are streamlined.
- 2. Parameter estimation. The full mechanism involving the reactive intermediates involves both large and small rate constants, in which the large rate constants usually correspond to the reactions that consume the intermediates. The large rate constants corresponding to intermediate consumption reactions cannot easily be identified from experimental measurements. To identify these parameters, measurements of the rapidly evolving, low-concentration intermediates are required. In the reduced model, however, these large rate constants often are removed entirely or appear as ratios to other large rate constants. This change in parametrization of the model facilitates estimating the model parameters from slow-timescale measurements of only the high-concentration reactants and products that are typically available.
- 3. Model solution. The evolution of species concentrations is usually described by sets of nonlinear ordinary differential equations (ODEs) that must be solved numerically. Because of the large and small rate constants, the full model's ODEs are often stiff. Even in fortuitous cases in which the large rate constants were somehow available, early ODE solvers often failed to produce accurate solutions for the stiff equations generated by the full model. ODE solvers have improved to the point that even reasonably stiff ODEs corresponding to large, complex chemical mechanisms can be solved accurately. Simplifying the mechanism and reducing the stiffness may, however, lead to a large decrease in the required computation time.

The QSSA method has a long history and a prominent place in the education of chemists, biologists, and chemical and biological engineers. Although the validity of the QSSA model as an approximation to the full mechanism has been studied extensively [6, 10, 20, 21], some fundamental questions about the method have not been addressed. In this chapter, we first explore the following unanswered question: for what class of chemical reactions can the standard procedure for applying the QSSA actually be carried out? The answer to even this basic question is surprising.

We prove in Sect. 2 that the classic QSSA method cannot be carried out for chemical reactions as simple as those with second-order kinetics involving only three intermediates and two reactants and products. In Sect. 3, we consider two simple alternatives to the classical reduction method of the QSSA to overcome this limitation. We show that neither of these simple alternatives is sufficient for model reduction. In Sect. 4, we consider the numerical solution of the full and reduced models, and show how to rescale the species and parameters to obtain a tractable parameter estimation problem. In Sect. 6, we draw conclusions from this study and comment on future research directions.

2 The OSSA and Its Limitations

2.1 The QSSA Method

Reaction networks can involve the formation and consumption of intermediate species, which sometimes are transitory, highly reactive, and unlikely to exist outside the reaction mixture. The quasi-steady-state assumption in based on the rapid equilibration of these species. A slow-timescale model can be derived by setting the net rate of formation of these intermediates to zero. This results in a system of algebraic equations, which, if solved, provides expressions for the concentrations of the intermediates in terms of the reactant and product concentrations. Finally, this permits the construction of reaction-rate expressions for the stable reactants and stable products in terms of the reactant and product concentrations only.

We identify prospective highly reactive intermediates using characteristics such as a high rate of consumption, short lifetime, short induction time, or low concentrations. To see if a model reduction is appropriate for a given chemical mechanism, we also need to see how well the approximate solution obtained using the QSSA describes the exact solution. A detailed discussion of the selection of species in the QSSA and a list of references on this topic are given in [19].

We illustrate the OSSA approach using the following simple reaction network:

$$A \stackrel{k_1}{\rightleftharpoons} 2B$$
, $B \stackrel{k_2}{\longrightarrow} C$. (1)

The corresponding system of differential equations is

$$\dot{c}_{A} = -k_{1}c_{A} + k_{-1}c_{B}^{2},$$

$$\dot{c}_{B} = 2k_{1}c_{A} - 2k_{-1}c_{B}^{2} - k_{2}c_{B},$$

$$\dot{c}_{C} = k_{2}c_{B}.$$
(2)

Suppose that $k_2 \gg k_1$, so that the consumption rate of B is large compared with its rate of production; B is a highly reactive intermediate and a candidate for elimination. Setting the production rate of B to zero gives

$$R_{\rm B} = 2k_1c_{\rm A} - 2k_{-1}c_{\rm B}^2 - k_2c_{\rm B} = 0.$$
(3)

The reduced model for this example is obtained by solving this equation for $c_{\rm B}$ and substituting into the differential equations for A and C in (2). Here we select the single nonnegative solution for $c_{\rm B}$, but multiple nonnegative roots of QSSA algebraic systems are possible in general. In those cases, one usually selects the solution that leads to the reduced model which best fits the available data [23]. We call this procedure the standard approach to applying the QSSA. We obtain the system of differential equations

$$\dot{c}_{A} = -k_{1}c_{A} + k_{-1} \left(\frac{-k_{2} + \sqrt{k_{2}^{2} + 16k_{1}k_{-1}c_{A}}}{4k_{-1}} \right)^{2},$$

$$\dot{c}_{C} = k_{2} \cdot \frac{-k_{2} + \sqrt{k_{2}^{2} + 16k_{1}k_{-1}c_{A}}}{4k_{-1}},$$
(4)

which corresponds to the simple reaction

$$A \xrightarrow{\tilde{r}} 2C$$
, $\tilde{r} = \frac{k_2}{2} \left(\frac{-k_2 + \sqrt{k_2^2 + 16k_1k_{-1}c_A}}{4k_{-1}} \right)$.

Here, the \tilde{r} on top of the reaction arrow denotes a reaction rate function (and not a reaction rate constant). A comparison of the solutions to the differential equations (2) and (4) is depicted in Fig. 1. The rate constants used in the simulation were $k_1 = k_{-1} = 1$, $k_2 = 100$ and the initial conditions were $c_A(0) = 1$, $c_B(0) = c_C(0) = 0$. The two solutions are very close; the QSSA hypothesis for B is legitimate. Another lesson that is learned from model reduction by the QSSA is that *complex kinetics* (see the c_A dependence in the reaction rate \tilde{r}) can emerge from nothing more complicated than a few first- and second-order reactions when reactive intermediates are involved.

A key fact that allowed us to apply the QSSA was the possibility of explicitly solving equation (3) using a finite number of operations of addition, subtraction, multiplication, division, and radicals; explicit solutions of this kind are usually referred to as *solutions expressible by radicals*. While we are always able to solve quadratic equations explicitly, solutions expressible by radicals do not always exist for higher-degree polynomial equations. The next section reviews classical results that address this issue.

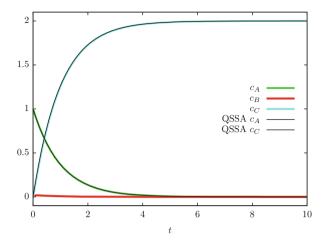


Fig. 1 The concentrations c_A and c_C with and without applying the QSSA to the intermediate B

2.2 Solvability by Radicals

It has been known since 1824, from the work of Niels Abel [1], that there is no formula expressible by radicals for the solution of the general fifth-degree polynomial equation. Around 1830, Évariste Galois produced his celebrated theory that gives a definitive answer to the question of solvability by radicals for any polynomial equation. In particular, this theory shows that the general polynomial equation of degree n cannot be solved using radicals for $any \, n > 5$.

Here, we introduce a few notions and theorems that will allow us to use the results of Galois theory. For an excellent overview of the subject, see [15]. The notions and facts about groups and fields presented below are standard and can be found in most textbooks on abstract algebra; see, for example, [14].

Consider the general polynomial equation of degree n,

$$a_n x^n + \ldots + a_1 x + a_0 = 0,$$
 (5)

with arbitrary coefficients a_0, \ldots, a_n in a field F. For our purposes, F will be the field generated by the coefficients of a polynomial whose roots we want to find. According to the overview of the QSSA in the previous section, we need to solve for the concentrations of intermediates in terms of the concentrations of nonintermediates. Thus our coefficients are not simply elements of the field $\mathbb Q$ of rational numbers; they may be polynomial expressions involving variables that represent concentrations of the nonintermediate species. Consequently, our field will be the smallest field that includes all these variables. This field is usually denoted by $\mathbb Q(c_1,\ldots,c_l)$, the set of quotients of real polynomials in the variables c_1,\ldots,c_l , representing the concentrations of the nonintermediate species. For instance, in the

example represented by Eq. (2), to find the concentration c_B we solved $2k_1c_A - 2k_{-1}c_B^2 - k_2c_B = 0$, viewed as an equation in c_B with coefficients in $\mathbb{Q}(c_A)$.

If the roots of Eq. (5) are not in F, there always exists a larger field that contains all these roots; let us denote these roots by x_{01}, \ldots, x_{0n} . The set of polynomials with variables x_1, \ldots, x_n and coefficients in the field F is denoted by $F[x_1, \ldots, x_n]$. A polynomial Q in $F[x_1, \ldots, x_n]$ that vanishes at the point (x_{01}, \ldots, x_{0n}) is called a *relation* among the roots of (5). Recall that the *symmetric group* S_n is the group of all permutations of n distinct elements.

Definition 1. The *Galois group* of the algebraic equation (5) over the field F is the subgroup of the symmetric group S_n consisting of the permutations of the roots (x_{01}, \ldots, x_{0n}) that preserve all the relations among these roots.

Galois theory introduces the key notion of a *solvable group*; for a detailed description of this notion, see [14]. The following theorem is the main result regarding solvability of algebraic equations by radicals.

Theorem 1. An algebraic equation of the form (5) is solvable by radicals if and only if its Galois group is solvable.

Therefore, the question of whether or not the solution of an algebraic equation can be made explicit using radicals is equivalent to checking a certain property of a group involving the coefficients of the equation. Most modern computer algebra software can handle the latter problem; we find the software package Maple [17] particularly suitable for this task.

It can be shown that the Galois group of the general polynomial equation of degree n with arbitrary coefficients is S_n . In view of Theorem 1, the nonsolvability by radicals of the general polynomial equation of degree ≥ 5 is then explained by the following result.

Theorem 2. The symmetric group S_n is solvable if and only if n < 5.

Before concluding this section, we shall mention another algebraic notion that we will use. Roughly speaking, a *Groebner basis* replaces a system of polynomial equations for *n* variables by a "nicer" one which has the same set of solutions as the first. For example, if the original system has a finite number of solutions (which will usually be the case for systems arising from chemical kinetics), we can choose a Groebner basis where one of the equations is a univariate polynomial in one of the variables. This way, we are able to address the problem of the explicit solvability of the initial multivariate polynomial system by using Galois theory on the univariate polynomial in the Groebner basis. A standard reference on Groebner bases is [7].

2.3 Nonsolvable Examples

As we saw above, a key step in the standard QSSA approach is solving a certain system of polynomial equations. But this is not always possible, and thus we are

confronted with an important limitation of this approach to applying the QSSA. In what follows, we present two chemical reaction networks where the standard QSSA approach cannot be used because of the nonsolvability by radicals of the resulting systems of algebraic equations.

The first example consists of the following mechanism:

$$2Y \xrightarrow[k_{-1}]{k_{-1}} 2B,$$

$$Y + B \xrightarrow{k_{2}} Z + A,$$

$$Z + B \xrightarrow[k_{-3}]{k_{-3}} 2X,$$

$$A + X \xrightarrow{k_{4}} Y + B,$$

$$2Z \xrightarrow{k_{5}} 2A,$$

whose dynamics is given by the equations

$$\dot{c}_{A} = k_{2}c_{B}c_{Y} - k_{4}c_{A}c_{X} + 2k_{5}c_{Z}^{2},$$

$$\dot{c}_{B} = 2k_{1}c_{Y}^{2} - 2k_{-1}c_{B}^{2} - k_{2}c_{B}c_{Y} - k_{3}c_{B}c_{Z} + k_{-3}c_{X}^{2} + k_{4}c_{A}c_{X},$$

$$\dot{c}_{X} = 2k_{3}c_{B}c_{Z} - 2k_{-3}c_{X}^{2} - k_{4}c_{A}c_{X},$$

$$\dot{c}_{Y} = -2k_{1}c_{Y}^{2} + 2k_{-1}c_{B}^{2} - k_{2}c_{B}c_{Y} + k_{4}c_{A}c_{X},$$

$$\dot{c}_{Z} = k_{2}c_{B}c_{Y} - k_{3}c_{B}c_{Z} + k_{-3}c_{X}^{2} - 2k_{5}c_{Z}^{2}.$$
(6)

To obtain fast equilibration of X, Y, and Z, we choose k_1 , k_{-3} , k_5 to be "large", k_{-1} , k_4 to be "small", and k_2 , k_3 to be of order O(1). Then the species X, Y, and Z are fast intermediates, and are candidates for the QSSA approach. Therefore, we need to solve the following system of algebraic equations for c_X , c_Y , and c_Z :

$$2k_{3}c_{B}c_{Z} - 2k_{-3}c_{X}^{2} - k_{4}c_{A}c_{X} = 0,$$

$$-2k_{1}c_{Y}^{2} + 2k_{-1}c_{B}^{2} - k_{2}c_{B}c_{Y} + k_{4}c_{A}c_{X} = 0,$$

$$k_{2}c_{B}c_{Y} - k_{3}c_{B}c_{Z} + k_{-3}c_{X}^{2} - 2k_{5}c_{Z}^{2} = 0.$$
(7)

We have used the software package Maple to generate a Groebner basis of this algebraic system. To facilitate the computation, we chose all the "large" reaction constants to be equal to K, the "small" ones equal to k, and all other reaction constants to be 1. An element of this basis was then found to be the univariate polynomial

$$P(c_{\rm Z}) = 32k^2c_{\rm B}^8K - 4k^3c_{\rm B}^6c_{\rm A}^2 - 2k^5c_{\rm B}^4c_{\rm A}^4 +$$
$$(-k^4c_{\rm A}^4c_{\rm B}^3 - 2k^2c_{\rm A}^2c_{\rm B}^5 - 16k^3Kc_{\rm B}^5c_{\rm A}^2)c_{\rm Z} +$$

$$(32k^{3}K^{2}c_{\rm B}^{4}c_{\rm A}^{2}+4k^{4}c_{\rm A}^{4}c_{\rm B}^{2}-64kK^{2}c_{\rm B}^{6}+4k^{2}Kc_{\rm A}^{2}c_{\rm B}^{4})c_{\rm Z}^{2}+\\(8K^{2}k^{4}c_{\rm A}^{4}c_{\rm B}+48k^{2}K^{2}c_{\rm B}^{3}c_{\rm A}^{2})c_{\rm Z}^{3}+\\(32K^{3}c_{\rm B}^{4}-16K^{3}k^{2}c_{\rm A}^{2}c_{\rm B}^{2}+8K^{3}k^{4}c_{\rm A}^{4}-256kK^{4}c_{\rm B}^{4})c_{\rm Z}^{4}-\\64K^{4}k^{2}c_{\rm A}^{2}c_{\rm B}c_{\rm Z}^{5}+\\(-128K^{5}k^{2}c_{\rm A}^{2}+256K^{5}c_{\rm B}^{2})c_{\rm Z}^{6}+\\512K^{7}c_{\rm A}^{8}.$$

Any c_Z that comes from a solution of the system (7) must also be a root of P. However, using Maple, we found that the Galois group over $\mathbb{Q}(c_A, c_B, k, K)$ of the equation $P(c_Z) = 0$ is S_8 . Hence, according to Theorem 1, c_Z cannot be found explicitly in terms of c_A and c_B . Therefore, the QSSA equations are not solvable this case.

Remark 1. To simplify the computations, we set all reaction rates equal to K, k, or 1 in the above calculations. On the other hand, if it were possible to find explicit formulas using radicals for the general set of parameters $k_1, k_{-1}, k_2, k_3, k_{-3}, k_4, k_5$, then the same formulas would apply for the special case of the parameters K, k, 1, which, according to the computations above, is impossible.

The second example is a real chemical mechanism for the photochemical decomposition of propanone,

$$CH_3COCH_3 \longrightarrow C_2H_6 + CO.$$

The following mechanism was proposed in [25]:

$$CH_{3}COCH_{3} \xrightarrow{k_{1} \atop k_{-1}} CH_{3}CO^{\bullet} + CH_{3}^{\bullet},$$

$$CH_{3}CO^{\bullet} \xrightarrow{k_{2} \atop k_{-1}} CH_{3}^{\bullet} + CO,$$

$$CH_{3}^{\bullet} + CH_{3}COCH_{3} \xrightarrow{k_{3} \atop M_{3}} CH_{4} + {}^{\bullet}CH_{2}COCH_{3},$$

$$CH_{3}^{\bullet} + CH_{3}^{\bullet} \xrightarrow{k_{4} \atop M_{3}} C_{2}H_{6},$$

$$CH_{3}^{\bullet} + {}^{\bullet}CH_{2}COCH_{3} \xrightarrow{k_{5} \atop M_{5}} CH_{3}CH_{2}COCH_{3},$$

$${}^{\bullet}CH_{2}COCH_{3} \xrightarrow{k_{7} \atop M_{5}} CH_{3}COCH_{2}CH_{2}COCH_{3},$$

$${}^{\bullet}CH_{2}COCH_{3} \xrightarrow{k_{7} \atop M_{7}} CH_{2}CO + CH_{3}^{\bullet},$$

$${}^{\bullet}CH_{2}COCH_{3} \xrightarrow{k_{8} \atop M_{7}} CH_{2}COCH_{3}.$$

To simplify the notation, we write

A = CH₃COCH₃, B = CO, C = C₂H₆, D = CH₄, E = CH₃CH₂COCH₃,
$$F = CH_3COCH_2CH_2COCH_3, G = CH_2CO,$$
$$H = CH_3COCOCH_3, X = CH_3CO^{\bullet}, Y = CH_3^{\bullet}, Z = {}^{\bullet}CH_2COCH_3.$$

The corresponding system of differential equations is

$$\dot{c}_{A} = -k_{1}c_{A} + k_{-1}c_{X}c_{Y} - k_{3}c_{A}c_{Y},
\dot{c}_{B} = k_{2}c_{X},
\dot{c}_{C} = k_{4}c_{Y}^{2},
\dot{c}_{D} = k_{3}c_{A}c_{Y},
\dot{c}_{E} = k_{5}c_{Y}c_{Z},
\dot{c}_{F} = k_{6}c_{Z}^{2},
\dot{c}_{G} = k_{7}c_{Z},
\dot{c}_{H} = k_{8}c_{X}^{2},
\dot{c}_{X} = k_{1}c_{A} - k_{-1}c_{X}c_{Y} - k_{2}c_{X} - 2k_{8}c_{X}^{2},
\dot{c}_{Y} = k_{1}c_{A} + k_{2}c_{X} - k_{-1}c_{X}c_{Y} - k_{3}c_{A}c_{Y} - 2k_{4}c_{Y}^{2} - k_{5}c_{Y}c_{Z} + k_{7}c_{Z},
\dot{c}_{Z} = k_{3}c_{A}c_{Y} - k_{5}c_{Y}c_{Z} - 2k_{6}c_{Z}^{2} - k_{7}c_{Z}.$$
(8)

The prospective QSSA intermediates are the radicals X, Y, and Z. The algebraic system in c_X , c_Y , and c_Z is

$$k_{1}c_{A} - k_{-1}c_{X}c_{Y} - k_{2}c_{X} - 2k_{8}c_{X}^{2} = 0,$$

$$k_{1}c_{A} + k_{2}c_{X} - k_{-1}c_{X}c_{Y} - k_{3}c_{A}c_{Y} - 2k_{4}c_{Y}^{2} - k_{5}c_{Y}c_{Z} + k_{7}c_{Z} = 0,$$

$$k_{3}c_{A}c_{Y} - k_{5}c_{Y}c_{Z} - 2k_{6}c_{Z}^{2} - k_{7}c_{Z} = 0.$$
(9)

If we choose all reaction rate parameters to be 1, then this system has a Groebner basis that contains the following univariate polynomial in c_z :

$$R(c_{\rm Z}) = -c_{\rm A}^5 + c_{\rm A}^6 + (5c_{\rm A}^4 - 4c_{\rm A}^5)c_{\rm Z} + (-12c_{\rm A}^3 - 4c_{\rm A}^5 + c_{\rm A}^2 + 5c_{\rm A}^4)c_{\rm Z}^2 + (-16c_{\rm A}^3 + 16c_{\rm A}^2 - 2c_{\rm A} + 8c_{\rm A}^4)c_{\rm Z}^3 + (4 + 42c_{\rm A}^2 - 4c_{\rm A} - 8c_{\rm A}^3 + 4c_{\rm A}^4)c_{\rm Z}^4 + (44c_{\rm A}^2 + 20)c_{\rm Z}^5 + (44 + 8c_{\rm A} + 20c_{\rm A}^2)c_{\rm Z}^6 + 48c_{\rm Z}^7 + 24c_{\rm Z}^8.$$

As in the previous example, the Galois group of the polynomial $R(c_Z)$ over the field $\mathbb{Q}(c_A)$ is S_8 . Therefore c_X, c_Y , and c_Z cannot be expressed in terms of c_A , i.e., the QSSA approach is not solvable in this case.

2.4 Challenges in the Characterization of Systems to Which the Standard QSSA Procedure Can Be Applied

The method described in the previous section can be extended to an algorithm for checking whether the standard QSSA procedure can be applied to a generic system. With all rate constants regarded as symbolic entries, Groebner bases are computed using appropriate monomial orderings, and univariate polynomials are obtained for each intermediate. If all corresponding Galois groups are solvable, we conclude that the standard QSSA procedure may be applied. If at least one such group is not solvable, then the standard QSSA procedure cannot be carried out.

On the other hand, calculations of Groebner bases are combinatorially explosive even for polynomials over real numbers, and are even more computationally expensive over fraction fields with several variables. Therefore, for large enough networks, the computation may not terminate. Moreover, even if the computation terminates and the standard QSSA procedure can be applied, constructing the actual equations of the reduced model may involve further complications, including convoluted algebraic expressions whose signs need to be analyzed, and the possibility of multiple nonnegative roots of the QSSA algebraic system.

Setting some rate constants to simple numerical values, as we have done above, can reduce dramatically the computational size of the problem. However, while this easier problem may be computationally tractable, it is only informative if one of the resulting Galois groups is *not* solvable. In that case we can conclude that the QSSA procedure cannot be applied to the system with general reaction rates. On the other hand, even if all resulting Galois groups are solvable for some fixed reaction rate values, we cannot conclude that the system with general reaction rates is solvable.

3 Alternatives to Solving the QSSA Equations

3.1 Eliminating Reactions Involving Intermediates

The goal in QSSA model reduction is usually not to *evaluate* the concentrations of the intermediates but to *eliminate* them from the reduced model. We next investigate whether there is a general method to remove them short of solving for them. Consider first an example in which this elimination can be done:

$$A \xrightarrow{r_1} B$$
, $B \xrightarrow{r_2} C$.

We do not assume any simple form for the rate expressions. If B is an intermediate, we set its production rate to zero and obtain

$$R_{\rm B} = r_1(c_{\rm A}) - r_2(c_{\rm B}) = 0.$$

This relationship defines c_B as an implicit function of c_A , but we assume that the algebraic complexity of the function r_2 prevents solving this equation explicitly. For this simple example, knowing only that $r_2(c_B) = r_1(c_A)$ is sufficient. In fact, the production rates of A and C using $r_2 = r_1$ are expressible by

$$R_{\rm A} = -r_1({\rm A}), \qquad R_{\rm C} = r_1({\rm A}),$$

and we have eliminated B and any large rate constants from the model without solving explicitly for c_B as a function of c_A , i.e., $c_B(c_A)$.

But now consider a slightly more complex example:

$$A \xrightarrow{r_1} 2B$$
, $2B \xrightarrow{r_2} D$, $B + C \xrightarrow{r_3} E$.

If we say B is an intermediate again, we have

$$R_{\rm B} = 2r_1(c_{\rm A}) - 2r_2(c_{\rm B}) - r_3(c_{\rm B}, c_{\rm C}) = 0.$$

In general, this equation implicitly defines a function $c_B(c_A, c_C)$, but we again assume that we cannot solve for this function explicitly. The production rates of the reactants and products are as follows:

$$R_{\rm A} = -r_1(c_{\rm A}), \qquad R_{\rm C} = -r_3(c_{\rm B}, c_{\rm C}), \qquad R_{\rm D} = r_2(c_{\rm B}), \qquad R_{\rm E} = r_3(c_{\rm B}, c_{\rm C}).$$

To eliminate B from the model, we require r_2 and r_3 . But the QSSA relation provides only the relation $2r_1 - 2r_2 - r_3 = 0$. We can remove r_2 or r_3 from the model using this equation, but not both. We require the function $c_B(c_A, c_C)$ to substitute into r_2 and r_3 in order to remove B from the reduced model in this example. Eliminating reactions is not a general procedure. If the number of reaction rate expressions in which intermediates appear exceeds the number of intermediates, we do not obtain enough equations to eliminate the intermediates. In the preceding example, we have one intermediate (B), but it appears in two reaction rate expressions (r_2, r_3) .

The generalization of this idea of elimination to sets of reactions is known as the Horiuti–Temkin theory [13, 22]. We shall not discuss this generalization further here, because the second simple example shows that the Horiuti–Temkin theory is insufficient in general to eliminate the reaction rates containing intermediates as required to apply the QSSA.

3.2 Solving the Full or Reduced Model Numerically

Since we cannot solve the algebra of the QSSA and we cannot eliminate all reaction rates containing intermediates, we consider next the numerical solution of the full model. A simple approach is to set the rate constants corresponding to consumption of the intermediates large and solve the full model. We assume that the ODE solver can provide accurate solutions given any choice of large rate constants. Alternatively, one can replace the differential equations for the intermediates with the algebraic equations that result from setting their production rates to zero. This procedure produces a set of differential—algebraic equations (DAEs) in place of the ODEs of the full model. The procedure for generating and numerically solving these DAE models is known as computational singular perturbation (CSP). A discussion of the CSP method is provided in [16, 26, 27]. Whether one is numerically solving the full model or the reduced, slow-timescale DAE model, it is generally assumed that all kinetic parameters are known.

To illustrate the issues that arise when the large rate constants are not all known, we consider the following example:

$$A \xrightarrow{k_1} B$$
, $B \xrightarrow{k_2} C$, $2B \xrightarrow{k_3} D$, (10)

with the full model

$$\begin{split} \dot{c}_{\rm A} &= -k_1 c_{\rm A}, \\ \dot{c}_{\rm B} &= k_1 c_{\rm A} - k_2 c_{\rm B} - 2 k_3 c_{\rm B}^2, \\ \dot{c}_{\rm C} &= k_2 c_{\rm B}, \\ \dot{c}_{\rm D} &= k_3 c_{\rm B}^2. \end{split}$$

The production rate of B is given by

$$R_{\rm B} = k_1 c_{\rm A} - k_2 c_{\rm B} - 2k_3 c_{\rm B}^2. \tag{11}$$

Setting this production rate to zero and solving for c_B gives the QSSA result,

$$c_{\rm B} = \frac{2k_1/k_2}{1 + \sqrt{1 + \beta c_{\rm A}}} c_{\rm A}, \qquad \beta = 8k_1k_3/k_2^2.$$

We then express the production rates in terms of the concentrations of only the reactants and products (A, C, and D)

$$R_{\mathbf{A}} = -k_1 c_{\mathbf{A}},\tag{12}$$

$$R_{\rm C} = \frac{2k_1}{1 + \sqrt{1 + \beta c_{\rm A}}} c_{\rm A},\tag{13}$$

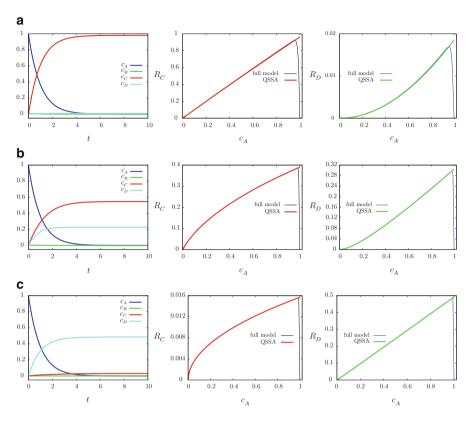


Fig. 2 Numerical solutions of the full model and QSSA approximation. *Left*: c_A , c_B , c_C , c_D versus time. *Middle*: R_C versus c_A . *Right*: R_D versus c_A . (a) $k_1 = 1$, $k_2 = 10^2$, $k_3 = 2 \times 10^2$, $\beta = 16 \times 10^{-2}$. R_C versus c_A is linear. (b) $k_1 = 1$, $k_2 = 10^2$, $k_3 = 2 \times 10^4$, $\beta = 16$. Neither R_C nor R_D is linear with c_A . (c) $k_1 = 1$, $k_2 = 10$, $k_3 = 2 \times 10^5$, $\beta = 16 \times 10^3$. R_D versus c_A is linear

$$R_{\rm D} = \frac{1}{2} k_1 \left(\frac{-1 + \sqrt{1 + \beta c_{\rm A}}}{1 + \sqrt{1 + \beta c_{\rm A}}} \right) c_{\rm A}. \tag{14}$$

If we were unable to solve the algebra, and instead tried the simple approach of setting all rate constants for consumption of intermediates large, we would set k_2 and k_3 large. But this does not specify the value of β . If we examine the two limiting cases of β large and β small, we obtain the production rates

$$eta
ightarrow 0, \qquad \qquad eta
ightarrow \infty, \ R_{\mathrm{A}} = -k_1 c_{\mathrm{A}}, \qquad R_{\mathrm{A}} = -k_1 c_{\mathrm{A}}, \ R_{\mathrm{C}} = k_1 c_{\mathrm{A}}, \qquad R_{\mathrm{C}} = 0, \ \label{eq:beta-condition}$$

$$R_{\rm D} = 0,$$
 $R_{\rm D} = \frac{1}{2} k_1 c_{\rm A}$

corresponding to the two reduced mechanisms

$$A \xrightarrow{k_1} C \quad (\beta \to 0), \qquad A \xrightarrow{k_1} \frac{1}{2} D \quad (\beta \to \infty).$$
 (15)

Some relevant numerical results for the example (10) are shown in Fig. 2. Notice that neither the limit $k_2 \gg k_3$ nor $k_3 \gg k_2$ can describe the behavior of the QSSA model for the intermediate range of β shown in Fig. 2b. We see that the QSSA treatment of the full model remains valid, but we cannot obtain the correct behavior by simply setting rate constants large. We need to know the relative sizes of some large rate constants; in this case, we need k_3/k_2^2 . It is a simple matter to estimate the parameters k_1 and β from measurements of C and D, but it is not a simple matter to know the form of the production rates of C and D given in Eqs. (13) and (14). The knowledge of the form of the production rates is the primary benefit of the standard QSSA in this simple example.

4 Rescaling Intermediates, and Parameter Estimation from Data

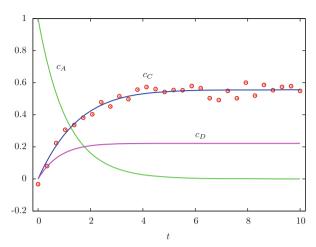
Since solving for the intermediates in closed form is not always possible, in this section we explore an alternative procedure of rescaling the intermediates. The choice of how to rescale is not unique, but we show in the next section how to automate the procedure for any kinetic model; a primary benefit is that the rescaling procedure often provides a tractable parameter estimation problem as well. For illustrative purposes, consider again the previous example, but assume that we are unable to solve the algebra to determine $c_{\rm B}$ from setting $R_{\rm B}=0$. Instead, we introduce a rescaled B concentration, denoted $c_{\rm Z}$, by writing

$$c_{\rm Z} = k_2 c_{\rm B}$$
.

Note that this choice is not unique. Setting $R_B = 0$ then adds an algebraic equation to the other species' differential equations. The reduced DAE model is

$$\begin{split} \dot{c}_{\rm A} &= -k_1 c_{\rm A}, \\ 0 &= k_1 c_{\rm A} - c_{\rm Z} - 2 K_3 c_{\rm Z}^2, \\ \dot{c}_{\rm C} &= c_{\rm Z}, \\ \dot{c}_{\rm D} &= K_3 c_{\rm Z}^2. \end{split}$$

Fig. 3 Measurement of the concentration of C versus time and prediction of the concentrations of A, B, and C from the rescaled model using optimal parameter estimates



Notice that the rescaling removes the two potentially large kinetic parameters k_2 and k_3 and introduces one new scaled parameter, $K_3 = k_3/k_2^2$. Without concentration measurements of reactants and products, we have no idea about the size of K_3 ; the low concentration of the intermediate B tells us only that k_3 or k_2 or both are large, and it is silent regarding the ratio k_3/k_2^2 .

Next, we attempt parameter estimation using both the full and the reduced models. Consider the data set with measurement noise depicted in Fig. 3. To make the parameter estimation problem challenging, we assume that only species C can be measured conveniently at the fairly slow sampling rate ($\Delta=0.34$) shown in the figure. This data set was generated from the full model using $k_1=1.0$, $k_2=100$, and $k_3=2\times10^4$, and the initial conditions $c_{A0}=1.0$ and $c_{B0}=c_{C0}=c_{D0}=0.0$. Note that these choices correspond to the intermediate case (b) in Fig. 2.

Normally distributed measurement noise (zero mean, standard deviation = 0.03) was added to the $c_{\rm C}$ of the full model to create the measurement set. Attempting to estimate k_1, k_2, k_3 of the full model from these data is hopeless. An optimizer would find a set of infinitely many estimates with approximately constant k_2/k_3^2 , and all points in this set would fit the measurements equally well. This lack of identifiability of parameters plagues all overly complex models using realistic measurement sets.

The estimates obtained for the parameters k_1 , K_3 of the reduced model are shown in Fig. 4. Notice that the parameters are well determined and that the approximate 95% confidence interval is small and contains the "true" parameters used to generate the data. The method used to generate the confidence interval is discussed in standard texts [3, 19]. The values of the estimates and the plus/minus interval (the bounding box of the ellipse shown in Fig. 4) are

¹Note that these are not quite the true parameter values, because we used the full model rather than the reduced model to generate the data.

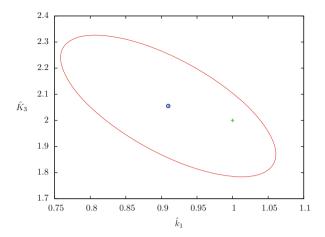


Fig. 4 Optimal parameter estimates \hat{k}_1 and \hat{K}_3 (\odot) based on the measurements of species C in Fig. 3, approximate 95% confidence interval (*line*), and parameter values used to create the measurements (+)

$$\begin{bmatrix} \hat{k}_1 \\ \hat{K}_3 \end{bmatrix} = \begin{bmatrix} 0.910 \\ 2.06 \end{bmatrix} \pm \begin{bmatrix} 0.151 \\ 0.271 \end{bmatrix}, \qquad \begin{bmatrix} k_1 \\ \frac{k_3}{k_2^2} \end{bmatrix} = \begin{bmatrix} 1.0 \\ 2.0 \end{bmatrix}.$$

As we can see, applying the QSSA to the full model provides a validated reduced model that is useful for other scientific studies and for engineering design purposes.

5 A Reparametrization of the QSSA Model

Recall the rescaling of intermediates presented in the previous section, where two kinetic parameters k_2 and k_3 were replaced by a single new parameter K_3 . In this section, we show how this rescaling procedure can be performed for any set of QSSA differential-algebraic equations, and highlight some interesting properties of the rescaled model.

Let (S) denote a system of DAEs corresponding to a QSSA model with unknown kinetic parameters and with variables x_1, \ldots, x_n . Suppose that the first m variables, x_1, \ldots, x_m , correspond to nonintermediate chemical species, and that the variables x_{m+1}, \ldots, x_n correspond to intermediate species. We assume that (S) fulfills the following assumption, which is satisfied by most QSSA systems encountered in practice: for any $t \ge 0$, if $x_1(t), \ldots, x_m(t)$ are known, then the n-m+1 algebraic equations of (S) have unique nonnegative solutions for $x_{m+1}(t), \ldots, x_n(t)$ (note that, as illustrated in Sect. 2.3, these solutions may not be expressible by radicals). As a consequence, a solution of (S) is determined by specifying only the first m coordinates of the initial condition vector.

In what follows, we devise a simpler model (\bar{S}) of (S) with variables $\bar{x}_1, \ldots, \bar{x}_n$ that captures the dynamics of the nonintermediate species x_1, \ldots, x_m . More precisely, (\bar{S}) will satisfy the following two properties:

- (i) (\bar{S}) has fewer parameters than (S);
- (ii) If $(x_1(t), \ldots, x_n(t))$ and $(\bar{x}_1(t), \ldots, \bar{x}_n(t))$, $t \ge 0$, are solutions of (S) and (\bar{S}) with $x_i(0) = \bar{x}_i(0)$ for all $i \in \{1, \ldots, m\}$, then $x_i(t) = \bar{x}_i(t)$ for all $i \in \{1, \ldots, m\}$ and all $t \ge 0$.

In other words, condition (ii) specifies that the outputs x_1, \ldots, x_m from (\bar{S}) and (S) corresponding to nonintermediates are the same.

5.1 Rescaling of the Intermediates

Our strategy is to consider rescalings of intermediates

$$\bar{x}_i = \alpha_i x_i \text{ for } i \in \{m+1, \dots, n\}$$
 (16)

that are "optimal" in the sense that the rescaled DAE system has the minimum number of parameters that can be obtained by any reparametrization of the form (16). More precisely, the α_i are chosen such that some monomials with unknown coefficients in (S) are replaced by monomials with coefficient 1 in the reparametrized system (\bar{S}) , and this is achieved for as many monomials as possible.

To illustrate, suppose that the DAE system (S) has intermediate variables x, y, z, w, u and suppose that the monomials of (S) involving the intermediate variables are

$$k_1xy$$
, k_2zw , k_3yz , k_4xw , k_5wu , and k_6yu .

Note that these monomials might contain more factors corresponding to nonintermediate variables, but, since these factors do not play a role in our analysis, we will neglect them.

Since the kinetic parameters k_1, \ldots, k_6 are unknown positive constants, we treat them as (linearly independent) symbolic indeterminates. Letting

$$\bar{x} = \alpha x$$
, $\bar{y} = \beta y$, $\bar{z} = \gamma z$, $\bar{w} = \delta w$, $\bar{u} = \eta u$,

the monomials become

$$\frac{k_1}{\alpha\beta}\bar{x}\bar{y}, \frac{k_2}{\gamma\delta}\bar{z}\bar{w}, \frac{k_3}{\beta\gamma}\bar{y}\bar{z}, \frac{k_4}{\alpha\delta}\bar{x}\bar{w}, \frac{k_5}{\delta\eta}\bar{w}\bar{u}, \frac{k_6}{\beta\eta}\bar{y}\bar{u}. \tag{17}$$

Let **C** denote the vector of the logarithms of the six coefficients in the monomials above, and let $\ln \mathbf{k}$, \mathbf{v} , and Ψ denote the 6×1 and 5×1 vectors and the 6×5 matrix, respectively, in the equality

$$\mathbf{C} = \ln \mathbf{k} - \Psi \mathbf{v} = \begin{bmatrix} \ln k_1 \\ \ln k_2 \\ \ln k_3 \\ \ln k_4 \\ \ln k_5 \\ \ln k_6 \end{bmatrix} - \begin{bmatrix} 1 & 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 1 & 0 \\ 0 & 1 & 1 & 0 & 0 \\ 1 & 0 & 0 & 1 & 1 \\ 0 & 1 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} \ln \alpha \\ \ln \beta \\ \ln \gamma \\ \ln \delta \\ \ln \eta \end{bmatrix} = \begin{bmatrix} \ln k_1 \\ \ln k_2 \\ \ln k_3 \\ \ln k_4 \\ \ln k_5 \\ \ln k_6 \end{bmatrix} - \begin{bmatrix} M_1 \cdot \mathbf{v} \\ M_2 \cdot \mathbf{v} \\ M_3 \cdot \mathbf{v} \\ M_4 \cdot \mathbf{v} \\ M_5 \cdot \mathbf{v} \\ M_6 \cdot \mathbf{v} \end{bmatrix}, \quad (18)$$

where M_j denotes row j of Ψ . The maximum number of zero coordinates for the vector \mathbf{C} equals $rank \Psi = 4$.

Since M_1 , M_2 , M_3 , and M_5 are linearly independent, we can make the corresponding coordinates of \mathbb{C} equal to zero (and therefore make the coefficients of the first two monomials in (17) equal to 1). We have

$$\mathbf{C} = \begin{bmatrix} \ln k_1 \\ \ln k_2 \\ \ln k_3 \\ \ln k_4 \\ \ln k_5 \\ \ln k_6 \end{bmatrix} - \begin{bmatrix} M_1 \cdot \mathbf{v} \\ M_2 \cdot \mathbf{v} \\ M_3 \cdot \mathbf{v} \\ (M_1 + M_2 - M_3) \cdot \mathbf{v} \\ M_5 \cdot \mathbf{v} \\ (M_1 + M_5 - M_4) \cdot \mathbf{v} \end{bmatrix} = \begin{bmatrix} \ln k_1 \\ \ln k_2 \\ \ln k_3 \\ \ln k_4 \\ \ln k_5 \\ \ln k_6 \end{bmatrix} - \begin{bmatrix} \ln k_1 \\ \ln k_2 \\ \ln k_3 \\ \ln k_1 + \ln k_2 - \ln k_3 \\ \ln k_1 + \ln k_2 - \ln k_3 \\ \ln k_5 \\ \ln k_1 + \ln k_5 - \ln k_4 \end{bmatrix}.$$

The new monomials

$$\bar{x}\bar{y}, \bar{z}\bar{w}, \bar{y}\bar{z}, K_1\bar{x}\bar{w}, \bar{w}\bar{u}, \text{ and } K_2\bar{y}\bar{u}$$
 (19)

contain only two parameters,

$$K_1 = \frac{k_4 k_3}{k_1 k_2}$$
 and $K_2 = \frac{k_6 k_4}{k_1 k_5}$.

In general, the number of new parameters is equal to the number of old parameters minus the rank of Ψ .

Remarks.

1. The reparametrized system (S) indeed satisfies the desired properties (i) and (ii). Condition (i) is true, as explained above. Also, the differential equations for $\bar{x}_1, \ldots, \bar{x}_m$ in (\bar{S}) are exactly the same as the corresponding differential equations for x_1, \ldots, x_m in (S); therefore, for identical initial conditions, the solutions must coincide, i.e., $\bar{x}_i = x_i$ for $i \in \{1, \ldots, m\}$.

2. Our example shows that the optimal scaling is not always obvious, and that, in general, the number of parameters that can be eliminated may be smaller than the number of intermediates present in the system.

3. Note that, in some cases, even after reducing the number of parameters as described above, we might not obtain a system with uniquely identifiable parameters. This may be the case even if there are no intermediate species; see [8] for examples. In future work, we will analyze this issue in more detail.

5.2 Equivalence of Reparametrizations

As explained above, the reparametrization (19) is optimal with respect to the number of parameters that it removes. However, this reparametrization is not the only one that is optimal. Similarly to the way M_1 , M_2 , M_3 , and M_5 determined an optimal reparametrization in the previous section, any choice of linearly independent rows of Ψ determines another optimal reparametrization.

Recall that the new parameters K_1 and K_2 in (19) are products of powers (positive or negative) of the original parameters k_1, \ldots, k_6 . This is true for any reparametrization. Interestingly, any two optimal reparametrizations of a system (\mathcal{S}), with parameter sets denoted \mathcal{P} and $\tilde{\mathcal{P}}$, are *parameter-set equivalent*, i.e., any element of $\tilde{\mathcal{P}}$ is a product of powers of elements of \mathcal{P} and vice versa.

For example, if we choose \mathbf{v} in (18) such that the second, fourth, fifth, and sixth coordinates of \mathbf{C} are zero (using the fact that M_2, M_4, M_5 , and M_6 are linearly independent), we have

$$\mathbf{C} = \begin{bmatrix} \ln k_1 \\ \ln k_2 \\ \ln k_3 \\ \ln k_4 \\ \ln k_5 \\ \ln k_6 \end{bmatrix} - \begin{bmatrix} (M_4 + M_6 - M_5) \cdot \mathbf{v} \\ M_2 \cdot \mathbf{v} \\ (M_2 + M_6 - M_5) \cdot \mathbf{v} \\ M_4 \cdot \mathbf{v} \\ M_5 \cdot \mathbf{v} \\ M_6 \cdot \mathbf{v} \end{bmatrix} = \begin{bmatrix} \ln k_1 \\ \ln k_2 \\ \ln k_3 \\ \ln k_4 \\ \ln k_5 \\ \ln k_6 \end{bmatrix} - \begin{bmatrix} \ln k_4 + \ln k_6 - \ln k_5 \\ \ln k_2 \\ \ln k_2 + \ln k_6 - \ln k_5 \\ \ln k_4 \\ \ln k_5 \\ \ln k_6 \end{bmatrix},$$

and the new monomials are

$$\tilde{K}_1 \bar{x} \bar{y}$$
, $\tilde{K}_2 \bar{z} \bar{w}$, $\bar{y} \bar{z}$, $\bar{x} \bar{w}$, $\bar{w} \bar{u}$, and $\bar{y} \bar{u}$,

where

$$\tilde{K}_1 = \frac{k_1 k_5}{k_4 k_6}$$
 and $\tilde{K}_2 = \frac{k_3 k_5}{k_2 k_6}$.

Note that $\tilde{K}_1 = 1/K_2$ and $\tilde{K}_2 = K_1/K_2$, and the two reparametrizations are indeed parameter-set equivalent.

5.3 Propanone Example

We shall now illustrate the usefulness of the reparametrization discussed in this section by estimating parameters for the photochemical decomposition of propanone. A representative data set was generated from the full model described by (8) using $k_1 = 10^{-2}, k_{-1} = 10^7, k_2 = 10^3, k_3 = 10^2, k_4 = 5 \times 10^4, k_5 = 10^3, k_6 = 10^1,$ $k_7 = 10^{-1}, k_8 = 10^9, c_{A0} = 1, c_{B0} = c_{C0} = c_{D0} = c_{E0} = c_{F0} = c_{G0} = c_{C0}$ $c_{\rm H0} = c_{\rm X0} = c_{\rm Y0} = c_{\rm Z0} = 0$. These parameter values were chosen so that the major products and reactants A, B, C, D, and H would be present in larger amounts than the minor species E, F, and G, and the reactive intermediates X, Y, and Z would be present in much smaller quantities. Normally distributed measurement noise (zero mean, variance = 10^{-5}) was added to c_A , c_B , c_C , c_D , c_E , c_F , c_G , and c_H to create the measurement set. Similarly to the example represented by Eq. (10), estimating all nine parameters of the full model would result in infinitely many parameter sets which fit the data equally well. The reparametrized DAE model had six (rescaled) parameters k_1 , $K_{-1} = k_{-1}/(k_2k_3)$, $K_4 = k_4/k_3^2$, $K_5 = k_5/(k_3k_7)$, $K_6 = k_6/k_7^2$, and $K_8 = k_8/k_2^2$, which were estimated using the software package parest dae to obtain a good fit to the measurement data and to obtain reasonably small 95 % confidence intervals containing the "true" parameters used to create the measurement data. Figure 5 shows the fit between the measurement data and the estimated solution. The Estimated values of the rescaled parameters and their corresponding confidence intervals are

$$\begin{bmatrix} \hat{k}_1 \\ \hat{K}_{-1} \\ \hat{k}_4 \\ \hat{k}_5 \\ \hat{K}_6 \\ \hat{k}_8 \end{bmatrix} = \begin{bmatrix} 0.0099 \\ 98.4 \\ 5.03 \\ 101 \\ 993 \\ 996 \end{bmatrix} \pm \begin{bmatrix} 0.0017 \\ 82 \\ 0.39 \\ 5.03 \\ 76 \\ 68 \end{bmatrix}, \qquad \begin{bmatrix} k_1 \\ K_{-1} \\ K_4 \\ K_5 \\ K_6 \\ K_8 \end{bmatrix} = \begin{bmatrix} 0.01 \\ 100 \\ 5 \\ 100 \\ 1000 \\ 1000 \end{bmatrix}.$$

Note that the confidence interval for the parameter \hat{K}_{-1} is the largest in a relative sense, indicating that this parameter is the least well determined by this experiment. If this uncertainty were deemed too large, one could then apply experimental design methods to determine the optimal experiment to be performed next in order to provide more information about this parameter [2, 19]. This example shows, however, that although estimation of all of the parameters of the full model is not possible, reparametrization of the corresponding DAE model allows us to identify all of the parameters of the reparametrized DAE model. The reduced model is perfectly adequate for predicting the concentrations of all measurable species. If one were interested in identifying all of the full model's rate constants, different experiments using measurements of the QSSA species would be required.

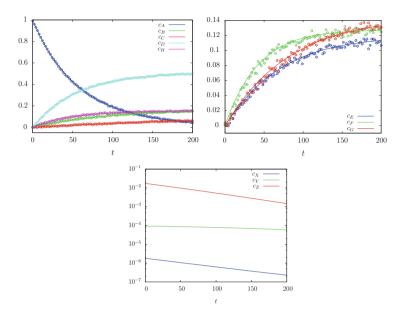


Fig. 5 Measurements of major and minor species and predictions of all species by the reduced DAE model. Top left: concentrations of major species c_A , c_B , c_C , c_D , c_H versus time. Top right: concentrations of minor species c_E , c_F , c_G versus time. Bottom: concentrations of reactive intermediates c_X , c_Y , c_Z versus time

6 Conclusions

The 100-year-old approach of classic QSSA model reduction, as taught in introductory courses, cannot be carried out for many relevant kinetics problems. We have proved that the algebra cannot be solved for even as few as five reactions involving five species (with three intermediates) with nothing more complex than bimolecular mass action kinetics. If any readers can find simpler nonsolvable examples, the authors would like to know about them. We have also analyzed a chemical mechanism taken from the literature and shown that it cannot be reduced by the classical approach. We have described algorithms that can test any mechanism for solvability. We have shown that the alternative approach of the Horiuti–Temkin theory also does not achieve the requirements of model reduction.

The first goal of this chapter was simply to make instructors aware of the limitations of trying to apply the QSSA in this way. Students should probably be told of these limitations when they are introduced to the approach. A second, longer-term goal was to promote the idea of *rescaling* the low-concentration species rather than solving for them. Although the choice of the rescaled parameters is not unique, the minimum number of rescaled parameters remaining in the reduced model *is* unique, and all reduced models with this minimum number of rescaled

parameters are equivalent. We expect that in most large enough examples, one cannot solve the QSSA equations explicitly using radicals. Moreover, even when one can solve them explicitly, it may still be preferable to use rescaling in order to identify key combinations of parameters which can be identified from data. The result of the procedure can be a reduced (DAE) model with rescaled parameters that are identifiable from standard measurements. Calculations using the open source software package parest_dae that estimates parameters and confidence intervals for DAE models were presented. This package makes use of the recently released SUNDIALS implicit ODE solver IDAS [12].

Looking to the future, as ab initio methods for predicting rate constants become more capable, we may be able to reduce the number of large rate constants and functions of these large constants that must be estimated from measurements. Model validation studies may then be carried out numerically with the full model, rather than by inspecting the reduced model's structural dependence on large-concentration reactants and products. Further research and tool development supporting both rate constant prediction and numerical model validation should prove highly useful to scientists developing and using complex chemical models.

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